

CONSTANTINESCU, O.

Some new micromycetes identified in Rumania. p. 453.

COMUNICARILE. Bucuresti. Vol. 9, no. 5, May 1959.

Monthly List of East European Accessions (EEAI) IC, Vol. 9, no. 1, January 1960.

Uncl.

CONSTANTINESCU, Ovidiu

Mycoflora of Rumania. Comunicare AR 11 no.6:679-687 Je '61.

1. Comunicare prezentata de Alice Savulescu, membru corespondent
al Academiei R.P.R.

CONSTANTINESCU, P.

About the decrease of the numbers of contacts by using bridge circuits. p. 45.
(SNALELE. SERIA STIINTELOR NATURII. Rumania. Vol. 5, no. 11, 1956)

SO: Monthly List of East European Accessions (KEAL) LC, Vol. 6, no. 7, July 1957. Uncl.

CONSTANTINESCU, P.

About the reduction of the number of contacts in introducing bridge circuits; direct conjugate conductivities. p. 399.
(STUDII SI CERCEATARI MATEMATICE. Rumania. Vol. 7, no. 3/4, July/Dec. 1956)

SO: Monthly List of East European Accessions (EAL) LC, Vol. 6, no. 7, July 1957. Uncl.

RUMANIA

NICOLAU, Cl., Conf. Dr., TOMAS, E.; OLINESCU, R.; CHRISTEA, Al., CONSTANTI-
NESCU, Rodica; and STROESCU, Eugenia

"Activity of 2-Methyl-1, 4-Naphthoquinone Sodium Bisulfite (Vitamin K3)
on Some Redox Enzymes"

Bucharest, Revista Sanitara Militara, Vol 16, Special No., 1965; pp 389-393

Abstract: In vitro studies to pinpoint mode of radiosensitizing effect of
Vitamin K3 in study with ceruloplasmin, catalase, peroxidase, d-amino-
acidoxidases. Results indicate that K3 vitamin has profound effect inhibit-
ing or potentiating the enzymatic activities depending on its concentration.
This is probably the mode of action of Vitamin K3 as radiosensitizer.

1/1

- 78 -

~~COMMISSIONER Radu~~ ✓
~~SURNAME (in caps); Given Names~~

Country: Rumania

Academic Degrees: Engineer

Affiliation: Member, Commission on Automation of the RFR Academy (Membru
in Comisia de Automatica a Academiei RFR).

Source: Bucharest, Stiinta si Tehnica (Supplement), No 4, 1961, pp 5.

Data: "The Home of the Cosmonaut."

CONSTANTINESCU, S.

SPIRCHEZ, T., Conf.; STOICHITA, S., dr.; MARINESCU, E., dr.; SCHIAU, S., dr.;
DULGERU, Carmen, dr.; ~~CONSTANTINESCU, S.~~; TACORIAN, S., dr.;
ALOMAN, Lucia, dr.; IONESCU, P.; STOICA, M.; CLEJAN, L.;
ALOMAN, N.

Physiopathology of dystonia of the afferent loop and of hepato-
biliary disorders in the gastrectomized. Med. int., Bucur. 9
no.2:231-247 Feb 57.

1. Lucrare efectuata in Clinica medicala si terapeutica nr.
V, Bucuresti (director, conf. T. Spirchez).

(GASTRECTOMY, complications
postop. afferent loop synd. & hepato-biliary disord.)
(GASTROINTESTINAL DISEASES
post-gastrectomy dystonia of afferent loop & hepato-
biliary disord.)
(LIVER DISEASES
post-gastrectomy hepato-biliary disord.)
(BILIARY TRACT, diseases
(SAME))

CONSTANTINESCO, R.

SPIRCHES, T., Conf.; STOICHITA, S., dr.; MARINESCU, E., dr.; SCHIAU, S.,
dr.; DULGHERU, C., dr.; CONESANINIESCU, S.; TACORIAN, S., dr.;
ALOMAN, L., dr.; IONESCU, F., dr.; STOICA, M., dr.; TACORIAN, L.,
dr.; ALOMAN, N., dr.

Clinical study of dystonia of the afferent loop and hepato-
biliary disorders in gastrectomized patients. Med. int., Bucur.
9 no.3:350-365 Mar 57.

1. Lucrare efectuata in Clinica a V-a medicala si terapeutica
Bucuresti, director conf. T. Spirchez.

(GASTRECTOMY, complications

postop. afferent loop synd., case reports)

(BILIARY TRACT, diseases

post-gastrectomy disorders, case reports)

CONSTANTINESCU, S.; TEODORESCU, B.; SANIELEVICI-MARINOV, S.; CUNESCU, V.; IACOB, A.; SCHMITZER, G.; VULCANESCU, M.; MARINOV, M.; VASILESCU, C.; LICHTENBERG, R.; BARCAN, F.; BANESCU, B.; BERNSTEIN, D.

Mass clinical and radiological detection (by radiophotography) of carditis in school-age children. Probl. reumat., Bucur. no.5:79-82 1958.

(RHEUMATIC HEART DISEASE, prevention & control
in school-aged child. in Rumania, clin. & radiol. diag.)

PARHON, C.I., acad.; CRACIUN, E., prof.; ASLAN, Ana, prof.; MAREA, Viorica;
VELCIU, V.; DAVID, I.; ZAHARIA, Maria; CONSTANTINESCU, Smaranda;
TASCA, C.; POPOVICI, M.

Tissular changes and lesions related to the pathology of the
aged. Romanian M. Rev. 3 no. 3:3-11 J1-S '59.
(GERIATRICS, pathology)

CRACIUN, E., prof.; ZAHARIA, Maria; CONSTANTINESCU, Smaranda; MARES, Viorica

Histochemical investigations in geriatrics. Rumanian M. Rev. 3
no.3:21-22 J1-S '59.

(METABOLISM in old age)

SPIRCHEZ, T., prof.; GHEORGHESCU, B.; MERCULIEV, E.; VOICULET, N.;
CONSTANTINESCU, S.; STOICHITA, S.; DULGHERU, C.; TACORIAN, S.;
RUSSU, M.

A study by means of radioactive isotopes of the blood volume and of
the exchanged between the peritoneal cavity and the blood in cirrhosis.
Rumanian M Rev. no.2:15-18 Ap-Je '60.

(LIVER CIRRHOSIS complications)

(BLOOD VOLUME)

(ASCITES etiology)

MANDACHE, Fl.; PRODESCU, V.; TEODORESCU, M.; CONSTANTINESCU, S.

Considerations on intestine transplants. Rumanian M Rev. no.4:63
O-D '60.

(INTESTINES transplantation)

KLEINERMAN, L. conf.; CONTANTINESCU, Anca, CONSTANTINESCU, Stela

Extra- and intra-cellular potassium changes in patients without edema treated with thiazides. Med. intern. (Bucur.) 10 no.5:557-561 My'64

1. Lucrare efectuata la A.S.C.A.R., Bucuresti (director: prof. C.C. Iliescu).

DUMITRESCU, Maria, dr.; GOIAESCU, Maria, dr.; SPINER, Frima, dr.; CONSTANTINESCU, S., dr.

On several cases of whooping cough and tuberculous meningitis with abdominal primary complex caused by a tubercle bacillus resistant to antibiotics. Med. int., Bucur. 12 no.1:111-117 Ja '60.

1. Lucrare efectuata in Clinica de boli contagioase I.M.F., Bucuresti, director: prof. M. Voiculescu.

(TUBERCULOSIS, MENINGEAL, complications)

(WHOOPING COUGH, complications)

(ANTITUBERCULAR AGENTS, therapy)

FRONESCU, E., dr.; PETRONIU, L., dr.; CONSTANTINESCU, S., chimist

Study of renal elimination of water during chronic hepatitis.
Med. int., Bucur. 12 no. 2: 269-277 P '60.

1. Incrare efectuata in Clinica a V-a medicala, I.M.F., Bucuresti.
(HEPATITIS, metabolism)
(WATER, metabolism)
(LIVER, metabolism)

MANDAKE, F.; PRODESCU, V.; CONSTANTINESCU, S.

Surgical treatment of rectal cancer. Khirurgiia 36 no.2:49-53
F '60.

(MIRA 13:12)

(RECTUM—SURGERY)

CONSTANTINESCU, S

MANDAKE, F. [Mandache, F.]; PRODESKU, V. [Prodescu, V.]; DZHILORTYANU, M.
[Djilortianu, M.]; KONSTANTINESKU, S. [Constantinescu, S.];
LUTSESKU, I. [Lucescu, I.]

Surgical treatment of peptic ulcer. Khirurgiia 36 no.12:61-66.
160. (MIRA 14:1)

1. Iz khirurgicheskoy kliniki bol'nitsy Brynkovenesk (sav. -
dotsent F. Mandake), Bukharest.
(STOMACH--SURGERY)

ZUGRAVESCU, I.; MOTOC, Florica; CONSTANTINESCU, Smaranda; CONSTANTINESCU, C.

Biochemistry and histology of some experimental hepatic lesions.
Studii cerc biochimie 4 no.3:339-347 '61.

1. Institutul de anatomie patologica "Dr. V. Babes", Bucuresti.

+

SURNAME, Given Name

CONSTANINESCU, S.

Country: Rumania

Academic Degrees: -not given-

Affiliation: *)

Source: Timisoara, Timisoara Medical, Vol VI, No 1, Jan-Jun 1961, pp 33-37.

Data: "Reanimation in Terminal Collapse State With Transfusions of
Oxygenated Blood Through Artificial Heart-Lungs."

Authors:

MANDACHE, F.

MATEESCU, D.

PRODESCU, V.

KOVER, Gh.

ROSCA, S.

CIOPALA, E.

MATEICA, Monica

CONSTANTINESCU, S.

LUTESCU, I.

CANTARGIU, Sofia

TANCIU, I.

*) Work performed at the Surgical Clinic of "Brincovenesc" Hospital
(Clinica de Chirurgie a Spitalului "Brincovenesc"), Director: F.
MANDACHE.

GPO 981643

SPIRCHES, T., prof.; STOICHITA, S., dr.; TAGORIAN, S., dr.; RUSSU, M., dr.;
SCHIAU, S., dr.; CONSTANTINESCU, S., chimist; GLEJAN, L., chimist;
BANDU, L., dr.

Secretory and motor disorders in the function of the operated stomach.
Med. intern., Bucur 13 no.2:201-210 F '61.

(GASTRECTOMY complications)
(STOMACH physiology)

MOTOC, Florica; CONSTANTINESCU, Smaranda

Capacity of liver transamination during the neoplastic process.
Studii cerc biochimie 5 no.1:91-95 '62.

1. Laboratorul de chimie al Institutului "Dr. V. Babes,"
Bucuresti.

BRUCKNER, Silvia, conf.; TEODORESCU, Tatiana, dr.; IOANESI, Iulia, dr.;
TEODORESCU, G., dr.; CONSTANTINESCU, S., dr.; COTARCEA, S., dr.;
ISBASESCU, C., chimiste; GARIBALDI, A.

The role of bacterial superinfection in the evolution of epidemic
hepatitis. Med. intern. 14 no.4:423-432 Ap '62.

1. Lucrare efectuata in Clinica de boli infectioase nr. 1, I.M.F.
(director: prof. M. Voiculescu).
(HEPATITIS, INFECTIOUS) (STAPHYLOCOCCAL INFECTIONS)
(STREPTOCOCCAL INFECTIONS) (PNEUMONIA) (OTITIS MEDIA)

MANDACHE, F.; PRODESCU, V.; CONSTANTINESCU, S.; KOVER, G.; STANCIULESCU, P.

Sympathectomy associated with adrenalo-cementopexy. A method for portal derivation of the circulation of the adrenal glands. Rumanian med. rev. no.2:63-70 '62.

(SYMPATHECTOMY) (ADRENAL GLANDS) (PORTAL SYSTEM)

ILIESCU, C.C., prof.; ROMAN, L., dr.; ILIESCU, M., dr.; IACOBINI, P., dr.;
NITU, S.; CONSTINTINESCU, S.; CONSTANTINESCU, A.; GHEORGHIU, C.

The action of unsaturated fatty acids on blood lipids in
arteriosclerosis. Med. intern. 14 no.12:1433-1442 D '62.

1. Lucrare efectuata la ASCAR, Bucuresti.
(BLOOD LIPIDS) (ARTERIOSCLEROSIS) (FATTY ACIDS)
(BLOOD CHOLESTEROL)

BRUCKNER, Silvia, conf.; TEODORESCU, Tatiana, dr.; TEODORESCU, Geta, dr.;
IOANESI, Iulia, dr.; CONSTANTINESCU, Sanda, dr.; COTARCEA, Sofia, dr.;
IZBASESCU, Aretia, chimist; GARIBALDI, Anastasia, chimist

Investigations concerning the factors determining the evolution of
epidemic hepatitis in children. The role of viral superinfections.
Med. intern. 15 no.2:179-184 F '63.

1. Lucrare afectuata in Clinica de boli contagioase I.M.F., Bucuresti.
(HEPATITIS, INFECTIOUS) (MEASLES) (MEASLES, GERMAN)
(CHICKENPOX) (MUMPS) (RESPIRATORY TRACT INFECTIONS)
(VIRUS DISEASES)

ILIESCU, N., dr.; DOMOCOS, G., dr.; IACOBINI, P., dr.; CONSTANTINESCU, S., chim.;
ILIESCU, C.C., prof.

Prolonged treatment with large doses of nicotinic acid in
coronary arteriosclerosis. Med. intern. 16 no.3:301-310
Mr*64.

1. Lucrare efectuata la A.S.G.A.R., Bucuresti.

*

ILIESCU, C.C., prof.; ILIESCU, Matei, dr.; ROMAN, L., dr.; IACOBINI, P., dr.;
CONSTANTINESCU, S., chimisti; NUTU, S.

The action of nicotinic acid on blood lipids in atherosclerosis.
Med. intern. 15 no.1:39-49 Ja '63.

1. Lucrare efectuata in Centrul de asistenta a cardiacilor A.S.C.A.R.,
Bucuresti.

(ARTERIOSCLEROSIS)
(BLOOD LIPIDS)

(NICOTINIC ACID)

ROMANIA

ILIESCU, C. C., Professor; ~~ILIESCU, Matei~~, MD; DOMOCOS, G., MD;
IACOBINI, P., MD; ~~CONSTANTINESCU, S.~~ Chemist; NIȚU, S.,
Chemist.

Bucharest, Viata Medicala, No 1, 1 Jan 64, pp 9-17

"Essential Hyperlipaemia Associated with Atherosclerosis
(Effects of Nicotinic Acid)."

(5)

MINAILESCU, V.V.; MIHESCU, R.; VINTILA, P.; BOGHEA, D.; GELSCO, E.;
CONSTANTINESCU, S.; CONSTANTINESCU, A.

~~Diagnostic value of changes of serum concentration of glutamic-oxalacetic transaminase in coronary disease. Stud. cercet. med. intern. 5 no.6:623-626 '64.~~

MANDACHE, Fl.; PRODUSCU, V.; TESODONESCU, M.; CONSTANTINESCU, S.;
VASILIU, M.

The place of broad gastric resection with gastroduodenal anas-
tomosis in the surgical treatment of gastroduodenal ulcer.
(Indications, contraindications, technique, immediate and late
results)..Rumanian med. rev. 19 no.1:58-64 Ap-Je'65.

POPA, I., ing.; SULER, S., ing.; GORAN, V., ing.; Constantinescu, S., ing.

Mechanizing concrete central stations. Rev constr si mat constr 15
no.10:529-535 0 '63.

1. Institutul de cercetari in constructii si economia constructiilor
(for Suler, Goran). 2. I.C.M.B. (for Constantinescu).

L 45248-66 T JK

ACC NR: AP6033594

SOURCE CODE: RU/0023/65/010/004/0373/0374

AUTHOR: Constantinescu, S. P. (Doctor)

ORG: Bacteriological Laboratory, ISIPM, Gaesti Raion (Laboratorul de bacteriologie ISIPM)

TITLE: Semiautomatic distributor of antibiotic powders and tablets required for antibiograms

SOURCE: Microbiologia, parazitologia si epidemiologia, v. 10, no. 4, 1965, 373-374

TOPIC TAGS: antibiotic, medication distributor

ABSTRACT: The author describes a simple device used for the distribution of antibiotic powder or tablets in specified amounts. The essential parts of the distributor are two polystyrene cylinders and a perforated disc. Orig. art. has: 1 figure. [JPRS: 32,913]

SUB CODE: 06 / SUBM DATE: 01Apr65

Card 1/1 *tdh*

UDC: 615.779.93-092.257:615.475

0920 1637

CONSTANTINESCU, S.P., dr.

Semi-automatic distributor for antibiotic powders or tablets
for antibiograms. Microbiologia (Bucur.) 10 no.4:373-374
Jl-Ag '65.

1. Lucrare efectuata in Laboratorul de bacteriologie al
I.S.I.P.M. raionul Gaesti, Regiunea Arges (director: dr.
E. Cioran).

RUMANIA.

576.85.07:535.24

ALTESCU, E. I., Dr, and CONSTANTINESCU, S. P., Dr. Work performed at the State Health Inspectorate of Gaesti Raion (Inspectoratul Sanitar de Stat) Arges Regiune.

"Photometric Measurement of Bacterial Growth."

Bucharest, Microbiologia, Parazitologia, Epidemiologia, Vol 11, No 6, Nov-Dec 66, pp 501-509.

Abstract [Authors' English summary modified]: The authors studied the influence of a number of factors on the photometric measurement of bacterial growth. Experimental results are presented to illustrate the variation of the results in terms of the optical path, the concentration, size and shape of the bacterial cells, the wave length and the refraction index of the cells.

Includes 3 figures and a bibliography with 43 entries, of which one Rumanian, 6 German, 7 Dutch and 29 English-language.
-- Manuscript submitted 5 April 1966.

CONSTANTINESCU, T.

Distr: 4E3d

⁷
Determination of mercaptans in gasoline. M. Constantinescu and T. Constantinescu. *Lucrări inst. petrol. se-
case București* 3, 353-53 (1957).—The decompn. of Fe-
(SCN)₃ in the presence of Ag mercaptide and the retention
of AgNO₃ and Ag₂O in the Ag mercaptide ppt. are the main
causes of inaccuracy in the volumetric detn. of mercaptans
in gasoline by the Volhard and Klason method.
R. D. Slăniceanu

5-
2 May
1

CONSTANTINESCU

Study of the catalytic synthesis of mercaptans from alcohols and hydrogen sulfide. M. Constantinescu and T. Constantinescu. *Petrol si Gaz* (Bucarest) 10, 298-303 (1959). The catalytic properties of the oxides of the elements of Group IV of the periodic system, Ti, Zr, Hf, and Th, for the production of mercaptans from alcs. and H₂S, were studied (TiO₂ was most efficient), and compared with SnO₂ and SiO₂ and Al₂O₃. The oxides of Group IVB, SnO₂, SnO, and probably PbO₂, were unsuitable. As the catalyst forms an ester with the alc. in the first stage, the acidity of the catalyst was of great importance. The more acid TiO₂ was therefore more efficient than the basic ThO₂, which under certain conditions formed unstable esters that were decompd. with H₂S. This was expl. proved. As best conditions for the formation of mercaptan were found: molar ratio of H₂S to alc. 1.5:1, gas velocity 175 per hr., temp. 316°. Under these conditions 72.6% of the alc. was used, 1% ethylene formed, and 5% H₂S decompd. Better yields were obtained with higher alcs. The thermodynamic calcn. of the equil. const. for various temps. were given.

V. Hoffmann

3
1- JAG (1/3)

Distr: 4E3d

/The partition of ethyl mercaptan and of a mercaptan mixture with distil. water, and by the same method the S mixture between sodium hydroxide solution and gasoline

capitan was... separatory funnel... for 2-3 hrs., with NaOH... gasoline phase... (50 cc) was decanted, and the residual mercaptan S was distd. by appn. with... of the mercaptans, and titration of the excess AgNO₃ with NH₄CNS, Pb(SO₄)₂, serving as indicator after a modified ASTM method reported earlier, cf. vol. 3, 1937. The gasoline itself should be free of mercaptans and naphthenic acids. In an aliquot of the NaOH soln. the mercaptans were liberated into gasoline by addn. of H₂SO₄, in another separatory funnel, kept in a cooling mixt., the strongly exothermic reaction... was finished

were as follows... EtSH and NaOH takes place in the... K is independent of the phase ratio... thus, the partition has a linear character; thus, the partition tests at 4 temps. yielded a log $K = 1.7$... detg. its equation and the value of $\Delta H = -7.5$... similar to that of other mercaptans. (c) In mercaptan mixts. the partition is no longer linear and the const. K increases with the initial amt. of mercaptan... not too large concns. the log $K = 1.7$... (e) In log coordinates, $\log C_2/\log C_1$ is... gasoline: in EtSH yields parallel straight lines... NaOH concn. while in mercaptan...

function of the values... phase ratio and... partition... and the curvature of the lines is a function of the variations of K (for larger amts. of partitioned mercaptan mixts. the equations are much more complicated as higher... of the influence of water...

R/007/61/012/001/003/003
A231/A126

AUTHORS: Constantinescu, M., Constantinescu, T. and Fedin, Tamara

TITLE: Contributions to the study of the catalytic condensing of ethylene with hydrogen sulfide

PERIODICAL: Petrol și Gaze, v. 12, no. 1, 1961, 33 - 43

TEXT: The article presents a solution regarding the production of ethylmercaptan from ethylene and H_2S with the aid of palladium and nickel sulfide catalysts. In a previous work: [Ref. 1: Constantinescu, M., and Constantinescu, T.: "Petrol și Gaze", no. 7, 1959, 298-304], the authors have shown that mercaptans can be produced by three method groups: i.e. by treating a neutral alkylic monoester ($R - SO_4Na$) with $NaSH$; from alkylic halogens ($R - Cl$) with NaS under pressure, and by catalytic methods. The catalysts allow a synthesis starting with reactants such as ethyl alcohol or ethylene, which directly lead to ethylmercaptan. In the above mentioned work (Ref. 1), the authors have studied the synthesis of mercaptans from lower alcohols. Since in the near future ethylene will be made from cracking gases or chemical reactions of methane, the study has been extended also on the synthesis of ethylene and hydrogen sulfide: $C_2H_4 + H_2S$

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Contributions to the study ...

R/007/61/012/001/003/003
A231/A126

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 \rightleftharpoons C_2H_5SH . According to the technical literature the photosynthesis with ultra-violet rays has also been studied before beside the above mentioned three methods. The majority of the publications refer to higher olefines, but not to ethylene. On the basis of the foreign literature, the authors have established that only the photochemical method supplied a higher efficiency (80%) for propylmercaptan at a temperature of $0^{\circ}C$. For ethylmercaptan the temperature is lower and the efficiency is negligible. The photochemical method, however, is very difficult to be applied in engineering, and needs an additionally catalyst. The only practical method is the catalytic method after having found a catalyst which supplies corresponding results at a temperature as low as possible and at usual pressure. The oldest examinations were carried out by H.R. Duffey in 1934, who used different catalysts and obtained a maximum ethylene transformation of 23.3% on a nickel catalyst. The task of this work is to find a highly efficient catalyst for the conversion of ethylene into ethylmercaptan. On the basis of the studied literature, the authors could establish that generally the catalysts, which supply a rather weak efficiency for the desired reaction, are the catalysts used also in hydrogenation and dehydrogenation reactions. For this purpose, this field has also been studied and proved to be the right way. A.W. Schultze's publication [Ref. 4: A.W. Schultze, J.P. Lyon, and G.H. Schort: "Ind. Eng. Chemis-

Card 2/3

Contribution to the study ...

R/007/61/012/001/003/003
A231/A126

try", Ibid: US 2,392.555; 40, 12, 1948] clearly shows that no higher mercaptan efficiency (66%) was obtained even in the presence of a catalyst, except in two recirculating stages with different catalysts for every stage and different pressures, i.e. 33 and 100 atm, when the reactants were partially in liquid phase. The authors' study was conducted to find a solution usable at ordinary pressure, to avoid technical complications, physical condensations, etc. This paper establishes the conditions and main parameters necessary for the transposition to the pilot or industrial scale. There are 5 tables, 1 figure and 9 references: 7 Soviet-bloc and 2 non-Soviet-bloc. The references to the English-language publications read as follows: Ref. 2: W.F. Vaughan, F.F. Rust, J. Evans: Org.Chem. 7,466,1942. Ref. 4: A.W. Schultze, J.P. Lyon, G.H. Schort: Ind. Eng. Chemistry Ibid.: U.S. 2,392.555; 40, 12, 1948.

SUBMITTED: August 29, 1960

Card 3/3

BERAL, H.; POPESCU, D.; CONSTANTINESCU, T.

Determination of 5,6-dimethylbenzimidazole. Rev chimie Min petr
13 no.1:54 Ja '62.

IONESCU, I.; ENACHE, St.; CONSTANTINESCU, T.

Contributions to the study of determination of the product
Cetazol. Rev chimie Min petr 14 no.9:534 S '63.

1. Institutul pentru controlul de stat al medicamentelor si
cercetari farmaceutice.

POPA, C.; CONSTANTINESCU, T.

Anticorrosive protection by enamel-chlorine-rubber in
the phosphorous fertilizer industry. Rev chimie Min petr
15 no. 5:298 My '64.

BERAL, H.; CONSTANTINESCU, T.

Determination of p-oxypropiofenone in H-365 phrenanthol tablets. Rev chimie Min petr 14 no.4:235-236 Ap '63.

1. Institutul pentru controlul de stat al medicamentelor si cercetari farmaceutice.

SOLOMON-IONESCU, Irina, farm.; ENACHE, Stefania, farm.; CONSTANTINESCU, T.,
chim.

Contributions to the study of quality conditions for cetazol
products. Farm Rum 11 no. 11:681-688 N°63.

1. Institutul pentru controlul de stat al medicamentului si
cercetari farmaceutice.

CONSTANTINESCU, T., ing.

Considerations of the specific aquifer potential of
the A aquifer horizon of the Fratesti Complex in the
zone of Bucharest. Meteorologia hidrol gosp 8 no.3:
124-127 '63.

CONSTANTINESCU, T.

FAGARAZANU, I. [Fagarasanu, I.] (Bukharest); KAPRINIZAN TS, (Bukharest);
BURLUI, D. (Bukharest); KONSTANTINESKU, TS. [Constantinescu, T]
(Bukharest)

Treatment of angina pectoris. Chirurgia 35 no.10:21-24 0 '59.

(MIRA 12:12)

(ANGINA PECTORIS surgery)

Gravimetric method for the determination of beryllium in the presence of other elements in alloys and minerals. Th. I. Pirtea and V. Constantinescu (Univ. "C. I. Parhon," Bucharest, Romania), *Z. anal. Chem.* 183, 183-8 (1959).
—In the presence of (ethylenedinitrilo)tetraacetic acid (I) Cu, Cd, Zn, Co, Ni, Fe, Al, Ti, Mn, Mg, Ca, Na, K, and NH_4^+ do not interfere in the pptn. of $[\text{Co}(\text{NH}_3)_4][(\text{H}_2\text{O})_2\text{Be}_2(\text{CO}_3)_2(\text{OH})_2] \cdot 3\text{H}_2\text{O}$. For the detn. of up to 75 mg. Be in 5-25 ml. of weakly acid soln. add 0.5-1 g. NH_4Cl and 0.5-2 g. I (more if large amts. of Fe^{+++} are present). If a ppt. forms, add 10% NH_4OH dropwise until the ppt. dissolves. Add 2-3 g. powd. $(\text{NH}_4)_2\text{CO}_3$. Add without mixing 0.5-2 ml. of $\text{Co}(\text{NH}_3)_4\text{Cl}$ soln. (II) and wait for the ppt. to start forming. Add an excess of II. Dil. the soln. so that the salt concn. is 2-3%, let stand for 1.5-2 hrs., and filter into a sintered crucible. Wash with 0.2% I. 3-4 times with 3-ml. portions 60% EtOH contg. a few drops 0.2% I. and finally with EtOH and Et_2O . Dry in a vacuum desiccator.

K. G. Steag.

Distr: 4E2c

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ABS. JOUR.	: RZKhim., No. 5 1960, No.	18700
AUTHOR	: Borza, A., Mueller, G., and Constantinescu, V.	
FROM	: Cluj Polytechnic Institute	
TITLE	: Investigation of the Possibility of the Application of Several New Materials in the Production of Metal-Bonded Abrasive Discs by Sintering	
ORIG. PUB.	: Lucrari Stiint Inst Politehn Cluj, 427-436 (1960)	
ABSTRACT	: The results from an investigation on the production of abrasive discs by the sintering of SiC and Cu powder mixtures at 1,100° under a methane atmosphere are presented. Discs of 45 and 100 mm diameter and thickness 1-1.3 mm were obtained and tested in the working of hard steel. The technological and economic advantages of the discs compared to Bakelite and rubber-bonded discs are discussed.	
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Co-authors:

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Abs Jour : Ref Zhur - Khimiya, No 5, 1959, No. 16510

Author : Szanto, A.; Cretu, V.; Constantinescu, V.

Inst : Not given

Title : Experience of the Kluzhskaya Oblast Apothecaries in the
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Orig Pub : Farmacia (Roman), 1957, 5, No 5, 442-455

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"Indications and Value of Considerations in Ligation of a Voluminous Hemangioma of the Left Side of the Liver, Operated by Subtotal Left Hepetactomy"

Bucharest, Revista Sanitara Militara, Vol 62, No. 3, May-June 1966;
pp 455-465

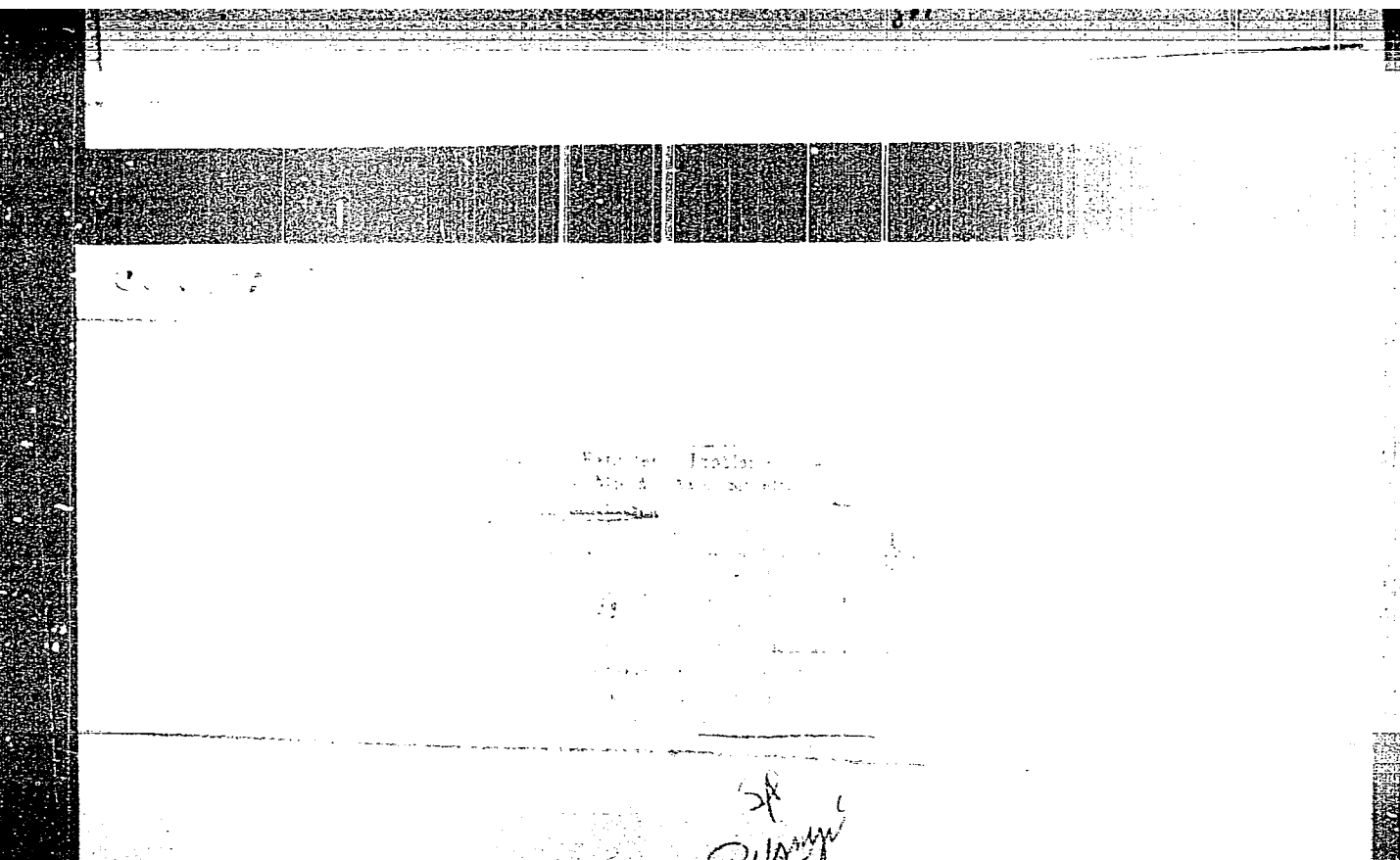
Abstract: Very detailed anatomical discussion of liver lobules and regional vasculature, leading to description of surgery in 39 year old soldier with liver tumor, a large cavernous hemangioma with satisfactory results and uneventful recovery. 3 anatomical diagrams, 4 photographs of operative stages, 1 photograph of surgical specimen, 1 photomicrogram, 1 liver scintigram with rose bengal. 10 Western, 16 Rumanian references. Manuscript received 10 February 1966.

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Uncl.

PHASE I BOOK EXPLANATION

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Cluj, Transylvania. Institutional Publications

Scientific Publications (Scientific Works) Cluj, Transylvania Publications, 1959.
677 p. Kramla ally inserted. No. of copies printed not given. No contributors mentioned.

NOTE: This book is intended for mathematicians, physicists, chemists, and civil and mechanical engineers.

CONTENTS: The book consists of 59 papers by Romanian specialists on problems in science and technology, particularly in mathematics, chemistry, physics, and engineering. The papers are divided into three sections: Mathematics, Physics, and Engineering. Each section contains several papers, with the number of pages for each given at the end of each article. Some of the articles are accompanied by references. No personalities are mentioned. At the back of the book there are 23 references, all Romanian.

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AUTHOR: Constantinescu, V.N.

TITLE: On the Motion Stability of Circular Bearings Lubricated With Gases

PERIODICAL: Studii si Cercetări de Mecanică Aplicată, 1959, Nr 1, pp 117 - 140 (RUM)

ABSTRACT: Because of disturbances produced especially at high speed operation of gas-lubricated circular bearings, more or less efficient solutions have been proposed already [Refs 1 and 2]. The author has conducted some theoretical studies with the purpose of obtaining some criteria for the determination of nonstable zones of gas-lubricated bearings and for the determination of the factors effecting an influence on these zones. For this purpose, it is necessary to know the motion in a nonpermanent region, i.e. in case the relative speed between the surfaces and the load supported by the bearing varies in time. The general equation of the lubrication with gases, written in the hypothesis of a certain polytropic evolution of the lubricating gas and in the usual condition of the problem of lubrication [Ref 3], is:

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$$\frac{\partial}{\partial x} \left(\frac{\partial \delta}{\partial x} \frac{p}{\mu} \right)^{\frac{1}{x} + 1} + \frac{\partial}{\partial z} \left(\frac{\partial \delta}{\partial z} \frac{p}{\mu} \right)^{\frac{1}{x} + 1} = 6 \left(\frac{1}{x} + 1 \right) \left\{ 2 (v_{2y} - v_{1y}) p^{\frac{1}{x}} - \right. \\ \left. - p^{\frac{1}{x}} \left[(v_{2x} - v_{1x}) \frac{\partial \delta}{\partial x} + (v_{2z} - v_{1z}) \frac{\partial \delta}{\partial z} \right] + \right. \\ \left. + \delta \left[\frac{\partial [p^{\frac{1}{x}} (v_{2x} + v_{1x})]}{\partial x} + \frac{\partial [p^{\frac{1}{x}} (v_{2z} + v_{1z})]}{\partial z} + 2 \frac{\partial p^{\frac{1}{x}}}{\partial t} \right] \right\}, \quad (1)$$

in which p = the pressure, δ = the thickness of the lubricant layer, x = the polytropic exponent of the evolution, and v_{1x}, v_{1y}, v_{1z} , respectively v_{2x}, v_{2y}, v_{2z} are the projections of the speeds V_1 and V_2 of both surfaces according to the reference directions x, y, z . The thickness of the lubricant film of circular bearings is given by:

$$\delta = \Delta + e \cos \theta = \Delta (1 + \alpha \cos \theta) \quad (2),$$

in which Δ is the radial clearance, e the excentricity, $\alpha = \frac{e}{\Delta}$ the relative excentricity, and the angle $\theta = \frac{x}{r}$. After determining the projections of the speed, the author establishes the equation of circular

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bearings:

$$\frac{\partial}{\partial t} \left(\frac{\partial^3 p}{\mu \partial \theta^3} \right) + r_1^2 \frac{\partial}{\partial z} \left(\frac{\partial^3 p}{\mu \partial z^3} \right) = 6 r_1^2 \left(\frac{1}{\delta} + 1 \right) \left(\Omega_1 + \Omega_2 \right) \frac{\partial (p \delta)}{\partial \theta} + 2 \dot{\psi} p \frac{\partial \delta}{\partial \theta} + 2 \frac{\partial (p \delta)}{\partial t} \quad (7)$$

considering that $V_0 = 0$. Ω_1 and Ω_2 are the revolution speeds. In the following paragraphs the author considers the case of a bidimensional motion in the lubricating layer and examines then the motion stability in the cases of a constant load and a centrifugal load. Since the pressure equation:

$$\frac{\partial}{\partial t} \left(\frac{\partial^3 p}{\mu \partial \theta^3} \right) = 12 r_1^2 \left[(\Omega_1 + \Omega_2) \frac{\partial (p \delta)}{\partial \theta} + 2 \dot{\psi} p \frac{\partial \delta}{\partial \theta} \right] \quad (8)$$

is very difficult to be solved, the author uses the method of disturbances recommended by J.S. Ausmann [Ref 4]. Considering that the pressure has the expression: $p = p_0 + \alpha p_1 + \alpha^2 p_2 + \dots$ (9)

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in which p_0 is a reference pressure, he derives the pressure distribution,

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limited only to the first two terms of (9):

$$p = p_0 + \frac{\alpha \xi \Delta \left(1 + \frac{2\psi}{\Omega_1 + \Omega_2}\right) p_0}{1 + \xi \Delta^2} (\xi \Delta + \sin \theta - \xi \cos \theta) \quad (17)$$

The resultants of the pressure in accordance with the direction of the lines of centers is:

$$P_t = - \int_0^{2\pi} p \cos \theta r_1 d\theta = \frac{\alpha \xi \Delta \left(1 + \frac{2\psi}{\Omega_1 + \Omega_2}\right) p_0 r_1}{1 + \xi \Delta^2} \quad (18)$$

and in accordance with the normal direction:

$$P_n = \int_0^{2\pi} p \sin \theta r_1 d\theta = \frac{\alpha \xi \Delta \left(1 + \frac{2\psi}{\Omega_1 + \Omega_2}\right) p_0 r_1}{1 + \xi \Delta^2} \quad (19).$$

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Considering that $\psi = -\Omega_1$ and $\Omega_2 = 0$, the author obtains for:

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$$p - p_0 = - \frac{\alpha \xi \Delta p_0}{1 + \xi^2 \Delta^2} (\xi \Delta + \sin \theta - \xi \Delta \cos \theta), \quad (20).$$

$$P_t = - \frac{\alpha \pi \xi \Delta^2 p_0 r_1}{1 + \xi^2 \Delta^2}; \quad P_n = - \frac{\alpha \pi \xi \Delta p_0 r_1}{1 + \xi^2 \Delta^2}$$

In this case the pressure resultants rotate together with the spindle and in the same direction: it is the case of a centrifugal load. This situation is somehow similar to the case of a lubrication with liquids [Ref 3]. Moreover, the analogy with the liquid lubrication is not complete, since in that case only the super-pressure zone is considered, which changes. If the normal speed of both surfaces is sufficiently reduced to neglect the influence of $\frac{\partial}{\partial t} (p^2 \partial)$, the results obtained for

permanent regions, affected by the factor $1 + \frac{2 \psi}{\Omega_1 + \Omega_2}$ (21)

can be used for dynamic regions. This conclusion permits the use of previously obtained results [Refs 6 and 7] for the computation of circular bearings. The author then establishes the equation of the motion stability of circular bearings, by using the method of small disturbances recommended

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by N. Tipei [Ref 3]: Considering a system of fix axes OXY and a mobile system $O_2x_2y_2$ with the origin in the bearing center (Figure 1), he obtains a compatibility condition of the equation system of motion: (Nr 22)

$$\left| \begin{aligned} &\Delta v^2 - (\dot{\gamma} - \dot{\gamma}^*)^2 \Delta + \frac{1}{m_1} \frac{\partial P_{1t}}{\partial \alpha} \left[2\alpha \Delta (\dot{\gamma} - \dot{\gamma}^*) + \frac{1}{m_1} \frac{\partial P_{1t}}{\partial \dot{\gamma}^*} \right] v - \frac{1}{m_1} \frac{\partial P_{1t}}{\partial \dot{\gamma}^*} \\ &- [2(\dot{\gamma} - \dot{\gamma}^*) v + \ddot{\gamma} - \ddot{\gamma}^*] \Delta - \frac{1}{m_1} \frac{\partial P_{1n}}{\partial \alpha} \alpha \Delta v^2 + \left(2\dot{\alpha} \Delta - \frac{1}{m_1} \frac{\partial P_{1n}}{\partial \dot{\gamma}^*} \right) v - \frac{1}{m_1} \frac{\partial P_{1n}}{\partial \dot{\gamma}^*} \end{aligned} \right| = 0 \quad (23)$$

in which $\dot{\gamma}^* = \dot{\gamma} - \dot{\varphi}$,
and the disturbance of the excentricity α and that of the angle $\dot{\gamma}$ are considered to be:

$$\delta \alpha = \alpha^* e^{v t}; \quad \delta \dot{\gamma}^* = \dot{\gamma}^{**} e^{v t} \quad (24)$$

In the determination (22) m_1 is the spindle mass, whereas P_{1t} and F_{1n} are the components on the directions t and n of the resultants of the pressure forces and external pressures. The determination (22) represents an equation of the 4th degree in v of the following shape:

$$C_0 v^4 + C_1 v^3 + C_2 v^2 + C_3 v + C_4 = 0 \quad (25).$$

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The conditions required by this system can be verified by the conditions of Routh-Hurwitz. The dynamic stability of the operation of a gas lubricated bearing can be appreciated if the values γ , α , Ω^* are known for the basic region and the forces P_1 , P_2 and their variation in ratio with α and Ω^* . The problem is determined if the derivatives of the pressure resultants in ratio with α , Ω^* , and $\dot{\Omega}^*$ are known. For the determination of these values the author considers the bidimensional motion and uses the conclusion of paragraph 1 and the results exposed in [Refs 6 and 7]. After determining the coefficients C_t and C_n by the Diagrams 2 and 3, and performing several other calculations, the author establishes the derivatives of the P_{pl} pressure resultant which interfere in the relation (22):

$$\frac{\partial P_{p1,t,n}}{\partial \alpha} = r_1 \left(1 + 2 \frac{\dot{\gamma} - \dot{\Omega}^*}{\Omega_1 + \Omega_2} \right) C_{t,n} \frac{\partial p_o}{\partial \alpha} + p_o r_1 \left(1 + 2 \frac{\dot{\gamma} - \dot{\Omega}^*}{\Omega_1 + \Omega_2} \right) \left[\frac{\partial C_{t,n}}{\partial \alpha} - \frac{\xi}{p_o} \frac{\partial C_{t,n}}{\partial \xi} \frac{\partial p_o}{\partial \alpha} \right]. \quad (43)$$

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$$\begin{aligned} \frac{\partial p_{p_1 t, n}}{\partial \dot{\vartheta}^*} &= r_1 \left(1 + 2 \frac{\dot{\vartheta} - \dot{\vartheta}^*}{\Omega_1 + \Omega_2} \right) c_{t, n} \frac{\partial p_o}{\partial \dot{\vartheta}^*} - \frac{2 p_o r_1}{\Omega_1 + \Omega_2} c_{t, n} - \\ &- r_1 p_o \left(1 + 2 \frac{\dot{\vartheta} - \dot{\vartheta}^*}{\Omega_1 + \Omega_2} \right) \frac{\xi}{p_o} \frac{\partial c_{t, n}}{\partial \xi} \frac{\partial p_o}{\partial \dot{\vartheta}^*} \end{aligned} \quad (43)$$

Considering p_o to be constant the above relations change into:

$$\begin{aligned} \frac{\partial p_{p_1 t, n}}{\partial \alpha} &= p_o r_1 \left(1 + 2 \frac{\dot{\vartheta} - \dot{\vartheta}^*}{\Omega_1 + \Omega_2} \right) \frac{\partial c_{t, n}}{\partial \alpha}, \\ \frac{\partial p_{p_1 t, n}}{\partial \dot{\vartheta}^*} &= - \frac{2 p_o r_1}{\Omega_1 + \Omega_2} c_{t, n} \end{aligned} \quad (44)$$

Considering p_o to be a function of α and $\dot{\vartheta}^*$, the relation (43) changes into:

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$$\left. \begin{aligned} \frac{\partial p_{1t,n}}{\partial \alpha} &= -p_0 r_1 \left(1 + 2 \frac{\dot{\theta} - \dot{\theta}^*}{\Omega_1 + \Omega_2} \right) \frac{c_{t,n}}{\chi} \frac{\partial \chi}{\partial \alpha} + p_0 r_1 \left(1 + 2 \frac{\dot{\theta} - \dot{\theta}^*}{\Omega_1 + \Omega_2} \right) \\ \left[\frac{\partial c_{t,n}}{\partial \alpha} + \frac{\xi'}{\chi} \frac{\partial c_{t,n}}{\partial \xi'} \frac{\partial \chi}{\partial \alpha} \right] &\approx p_0 r_1 \left(1 + 2 \frac{\dot{\theta} - \dot{\theta}^*}{\Omega_1 + \Omega_2} \right) \left(\frac{\partial c_{t,n}}{\partial \alpha} - \frac{c_{t,n}}{\chi} \frac{\partial \chi}{\partial \alpha} \right) \end{aligned} \right\} (45)$$

$$\frac{\partial p_{1t,n}}{\partial \dot{\theta}^*} = -\frac{2p_0 r_1}{\Omega_1 + \Omega_2} \xi' \frac{\partial c_{t,n}}{\partial \xi'}$$

The derivatives which interfere with (22) can be computed by these relations and the coefficients of the equation in (25) can be determined. The author then applies these results to the following two operational regions: constant load and centrifugal load. If p_0 is constant, the condition (28) can be expressed:

$$(c_1 c_2 - c_3) c_3 - c_1^2 c_4 \approx -c_1^2 c_4 < 0 \quad (53)$$

The motion of gas lubricated bearings of infinite extension with constant loads is unstable. But it is possible that the real situation should be

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more favorable, partially due to the fact that the finite extension could have a stabilizing effect and partially due to the introduced covering approximation. Some special constructional solutions are necessary to guarantee the motion stability. In case of a centrifugal load where $\Omega_2 = 0$, $j = -\Omega_1 = \text{constant}$, $\ddot{\eta} = 0$, $\dot{\eta}^* = \dot{\theta}^* = 0$, and the equation in $\sqrt{\xi}$ (54) is derived from (22), the condition (28) is expressed in a similar way as in the preceding case. If p_0 is variable, the motion is unstable for $\xi' > 1.4$, since the coefficient C_1 becomes negative. The more ξ' increases, this condition is not fulfilled since C_1 and C_2 tend towards 0. The motion stability can be achieved for some regions in function of ξ' , m_1 , Δ , but the motion becomes unstable at high ξ' values. The motion stability of air lubricated circular bearings is generally not guaranteed at especially high and very high speeds. The behavior is a little better in case of dynamic (centrifugal) loads, at average speeds and certain values for the masses in motion and for the relative dimensions of the bearings. The main factors causing the motion instability are the compressibility and especially the formation of depression zones in the lubrication stratum. To eliminate these deficiencies, the author recommends the use of multi-stage bearings [Ref 1], or the use of a lubricator feed under pressure

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[Ref 2]. In case of centrifugal loads at higher excentricities, the pehnomenon can be another one. Very high depressions and even negative pressures can appear which are physically not acceptable. In such cases the problem has to be reposed, considering $p \rightarrow 0$ in the regions where negative pressure would result.

There are: 10 graphs and 9 references, 2 of which are English, 2 French, 2 Rumanian, 2 Russian and 1 German.

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AUTHOR: Constantinescu, V.N., Engineer, Chief of Laboratory

TITLE: Air Lubricated Bearings

PERIODICAL: Metalurgia și Construcția de Mașini, 1959, Nr 11,
pp 959 - 966

ABSTRACT: The importance of gas lubricated bearings¹¹ increased during the last few years because of the following advantages: excellent behavior at very low, very high and average temperatures; low friction, thus enabling high revolution speeds, from 80,000 to 250,000 rpm; low operation temperature, approx 3-4°C at 30,000 - 40,000 rpm; low rate of wear. Gas lubricated bearings can operate for several 10,000 hrs [Ref 1]. The author briefly describes some operation principles of gas lubricated bearings, establishes the difference between gas lubricated

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and liquid lubricated bearings and explains the pressure distribution by appropriate equations. Gas lubricated bearings can be used in machines with very high revolution speeds, e.g. gyroscopes, centrifugal apparatus, spinning machines, glass cutting machines, grinding machines, etc. The pneumatic motor designed by the Institutul de Mecanică Aplicată al Academiei RPR (Institute of Applied Mechanics of the Rumanian Academy) with a speed of 56,000 rpm / Fig 15 / and the Soviet super-centrifugal apparatus with 22,000 rpm / Fig 16 / are equipped with gas lubricated bearings. Heavy machines, such as turbo-compressors, gas and steam turbines will be equipped with gas lubricated bearings in the near future. Gas lubricated bearings give excellent results at very low temperatures as, for instance in artificial satellites and rockets. They can also be used in measuring and control apparatus and installations. By using a pressure feed, a thin gas film can be produced between the

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surfaces at an operation speed of relatively zero.
[Ref 3]. There are 3 photos, 3 figures, 2 sets
of figures, 10 graphs and 9 Rumanian references.

ASSOCIATION: Secția de Mașini și Mecanisme, Institutul de Meca-
nică Aplicată, (Machine and Mechanism Section,
Institute of Applied Mechanics)

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CONSTANTINESCU, V.

Computation of bearings, composed of plane surfaces, lubricated in turbulent flow. p.755

STUDII SI CERCETARI DE MECANICA APLICATA. Academia Republicii Populare Romine
Bucuresti, Rumania
Vol. 10, no.3, 1959

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Uncl.

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AUTHORS: Constantinescu, V.N., and Marin, Gh.

TITLE: Pneumatic Motor With Air Lubricated Bearings

PERIODICAL: Studii si Cercetări de Mecanică Aplicată, 1960, No. 1, pp. 291-296

TEXT: For the experimental study of the operation of air lubricated bearings, the Institutul de mecanică aplicată (Institute of Applied Mechanics) designed a pneumatic motor with air lubricated bearings (Fig. 1). The rotor (1) is supported by two radial and two axial bearings. The active part of the rotor, the turbine, has been made by grinding some grooves into the rotor block. Two rotor types have been made, one conical (Fig. 1) and one cylindrical. The rotor is fed with compressed air through 13 nozzles, radially distributed in the casing (2). In case of a conical rotor, the casing is at the same time the axial bearing, fed under pressure. The second axial bearing (3) is made of a circular plane plate, provided with nozzles. The two radial bearings (4), (5) consist of a bushing each, assembled in a control system which allows a fastening of the bushings in position as close to the axis as possible, by tightening the nut (7) on the spherical surface of the intermediate bushing

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(16). The casing consists of two parts (9) and (10). The radial bearings have a diameter of 14 mm, a width of 28 mm and a radial tolerance of $1.2 \text{ }^{\circ}/\text{oo}$. The maximum lifting capacity of the air lubricated to a minimum thickness of the lubricating layer of $2 \text{ } \mu$ (Fig. 2). Each bearing can support 5 kg at 20,000 rpm and 10 kg at 60,000 rpm. The power consumption by friction is 4 w at 40,000 rpm and 10 w at 60,000 rpm (Fig. 3). Figure 3 also presents the power consumed by a bearing supposing that the bearing is completely unloaded and traced with a maximum load, equal to a minimum air lubricant layer of $2 \text{ } \mu$. Figure 4 shows the power consumption of the bearing No. 3, supposing that it is controlled for a tolerance of 0.1 mm or 0.5 mm respectively. Figure 5 shows the power consumption by friction of the apparatus at different rates of revolution. The radial bearings can also be fed under pressure. The motor has a stable operation, the maximum speed attained being 56,000 rpm. The operation is equally good in every position of the motor. The warming up is low. The radial bearings operate well also in case they are fed under pressure. Steel, bronze and cast iron has been used as bearing material. The installation will be used for

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